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Lecture 9 - Oblique Incidence of Electromagnetic Waves

I. Wave Propagation at an Arbitrary Angle

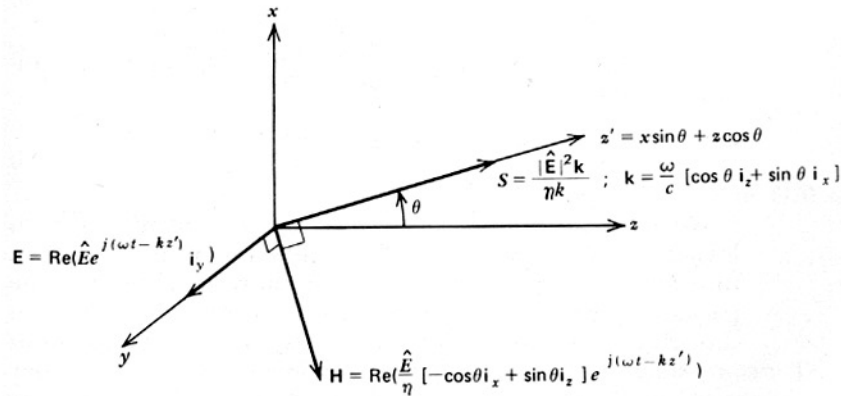


Figure 7-16 The spatial dependence of a uniform plane wave at an arbitrary angle θ can be expressed in terms of a vector wavenumber \mathbf{k} as $e^{-j\mathbf{k}\cdot\mathbf{r}}$, where \mathbf{k} is in the direction of power flow and has magnitude ω/c .

From *Electromagnetic Field Theory: A Problem Solving Approach*, by Markus Zahn, 1987. Used with permission.

$$z' = x \sin(\theta) + z \cos(\theta)$$

$$kz' = k_x x + k_z z, k_x = k \sin(\theta), k_z = k \cos(\theta), k = \omega \sqrt{\mu \epsilon}$$

$$\begin{aligned} \bar{E}(x, z, t) &= \text{Re} \left[\hat{E} e^{j(\omega t - kz')} \right] \bar{i}_y = \text{Re} \left[\hat{E} e^{j(\omega t - k_x x - k_z z)} \right] \bar{i}_y \\ \nabla \times \bar{E} &= -j\omega\mu \bar{H} \Rightarrow \bar{H} = -\frac{1}{j\omega\mu} \nabla \times \bar{E} = -\frac{1}{j\omega\mu} \left[-\bar{i}_x \frac{\partial E_y}{\partial z} + \bar{i}_z \frac{\partial E_y}{\partial x} \right] \\ \hat{H} &= -\frac{1}{j\omega\mu} \left[jk_z \hat{E} \bar{i}_x - jk_x \hat{E} \bar{i}_z \right] e^{-j(k_x x + k_z z)} \\ &= -\frac{\hat{E}}{\eta} [\cos(\theta) \bar{i}_x - \sin(\theta) \bar{i}_z] e^{-j(k_x x + k_z z)} \end{aligned}$$

$$\bar{H}(x, z, t) = \text{Re} \left[-\frac{\hat{E}}{\eta} (\cos(\theta) \bar{i}_x - \sin(\theta) \bar{i}_z) e^{j(\omega t - k_x x - k_z z)} \right]$$

In general:

$$\bar{k} = k_x \bar{i}_x + k_y \bar{i}_y + k_z \bar{i}_z \text{ is the wave vector}$$

$$\bar{r} = x \bar{i}_x + y \bar{i}_y + z \bar{i}_z \text{ is a position vector}$$

$$e^{-j\bar{k}\cdot\bar{r}} = e^{-j(k_x x + k_y y + k_z z)}$$

$$\nabla \left(e^{-j\bar{k}\cdot\bar{r}} \right) = -j(k_x \bar{i}_x + k_y \bar{i}_y + k_z \bar{i}_z) e^{-j\bar{k}\cdot\bar{r}} = -j\bar{k} e^{-j\bar{k}\cdot\bar{r}}$$

$$\nabla \rightarrow -j\bar{k}$$

$$\begin{aligned}
\nabla \times \hat{E} = -j\omega\mu\hat{H} &\Rightarrow -j\bar{k} \times \hat{E} = -j\omega\mu\hat{H} \\
&\quad \bar{k} \times \hat{E} = \omega\mu\hat{H} \\
\nabla \times \hat{H} = j\omega\epsilon\hat{E} &\Rightarrow -j\bar{k} \times \hat{H} = j\omega\epsilon\hat{E} \\
&\quad \bar{k} \times \hat{H} = -\omega\epsilon\hat{E} \\
\nabla \cdot \hat{E} = 0 &\Rightarrow -j\bar{k} \cdot \hat{E} = 0 \quad (\bar{k} \perp \hat{E}) \\
\nabla \cdot \hat{H} = 0 &\Rightarrow -j\bar{k} \cdot \hat{H} = 0 \quad (\bar{k} \perp \hat{H})
\end{aligned}$$

$$\begin{aligned}
\bar{k} \times (\bar{k} \times \hat{E}) &= \bar{k} \left(\bar{k} \cdot \hat{E} \right) - \hat{E} (\bar{k} \cdot \bar{k}) = \omega\mu (\bar{k} \times \hat{H}) = -\omega^2\epsilon\mu\hat{E} \\
|\bar{k}|^2 &= k_x^2 + k_y^2 + k_z^2 = \omega^2\epsilon\mu \\
\bar{A} \times (\bar{B} \times \bar{C}) &= \bar{B}(\bar{A} \cdot \bar{C}) - \bar{C}(\bar{A} \cdot \bar{B})
\end{aligned}$$

$$\begin{aligned}
\hat{S} &= \frac{1}{2}\hat{E} \times \hat{H}^*, \hat{H} = \frac{1}{\omega\mu}(\bar{k} \times \hat{E}) \\
\hat{S} &= \frac{1}{2}\hat{E} \times \left(\frac{1}{\omega\mu}\bar{k} \times \hat{E}^* \right) = \frac{1}{2\omega\mu} \left(\bar{k}(\hat{E} \cdot \hat{E}^*) - \hat{E}^*(\hat{E} \cdot \bar{k}) \right) \\
\hat{S} &= \frac{\bar{k}|\hat{E}|^2}{2\omega\mu} \quad (\hat{S} \text{ in the direction of } \bar{k})
\end{aligned}$$

II. Oblique Incidence Onto a Perfect Conductor

A. \bar{E} Field Parallel to Interface (TE - Transverse Electric)

$$\begin{aligned}
\bar{E}_i &= \text{Re} \left[\hat{E}_i e^{j(\omega t - k_{xi}x - k_{zi}z)} \bar{i}_y \right] \\
\bar{H}_i &= \text{Re} \left[\frac{\hat{E}_i}{\eta} (-\cos(\theta_i)\bar{i}_x + \sin(\theta_i)\bar{i}_z) e^{j(\omega t - k_{xi}x - k_{zi}z)} \right]
\end{aligned}$$

$$k_{xi} = k \sin(\theta_i), k_{zi} = k \cos(\theta_i), k = \omega\sqrt{\epsilon\mu}, \eta = \sqrt{\frac{\mu}{\epsilon}}$$

$$\begin{aligned}
\bar{E}_r &= \text{Re} \left[\hat{E}_r e^{j(\omega t - k_{xr}x + k_{zr}z)} \bar{i}_y \right] \\
\bar{H}_r &= \text{Re} \left[\frac{\hat{E}_r}{\eta} (\cos(\theta_r)\bar{i}_x + \sin(\theta_r)\bar{i}_z) e^{j(\omega t - k_{xr}x + k_{zr}z)} \right]
\end{aligned}$$

$$k_{xr} = k \sin(\theta_r), k_{zr} = k \cos(\theta_r)$$

Boundary conditions require that

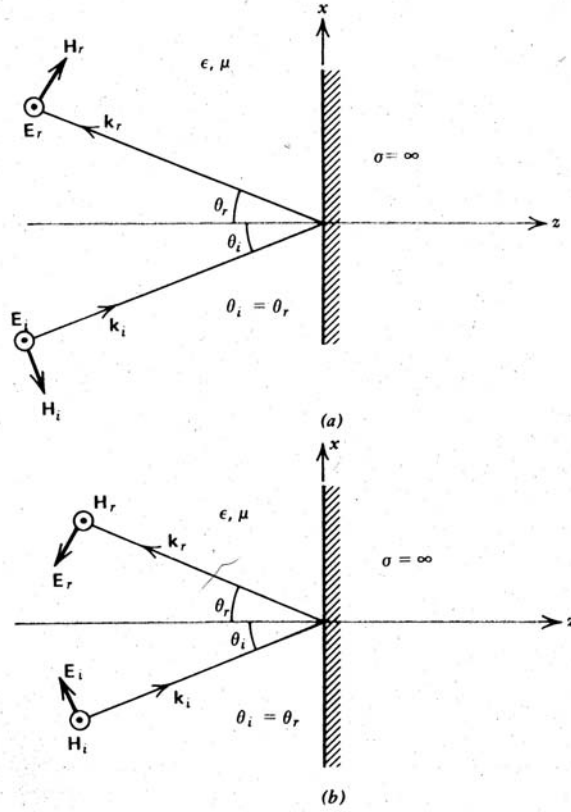


Figure 7-17 A uniform plane wave obliquely incident upon a perfect conductor has its angle of incidence equal to the angle of reflection. (a) Electric field polarized parallel to the interface. (b) Magnetic field parallel to the interface.

From *Electromagnetic Field Theory: A Problem Solving Approach*, by Markus Zahn, 1987. Used with permission.

$$\begin{aligned}
 \hat{E}_y(x, z = 0) = 0 &= \hat{E}_{yi}(x, z = 0) + \hat{E}_{yr}(x, z = 0) \\
 &= \hat{E}_i e^{-jk_{xi}x} + \hat{E}_r e^{-jk_{xr}x} = 0 \\
 \hat{H}_z(x, z = 0) = 0 &= \hat{H}_{zi}(x, z = 0) + \hat{H}_{zr}(x, z = 0) \\
 &= \frac{1}{\eta} \left(\hat{E}_i e^{-jk_{xi}x} \sin(\theta_i) + \hat{E}_r e^{-jk_{xr}x} \sin(\theta_r) \right) = 0 \\
 k_{xi} = k_{xr} &\Rightarrow \sin(\theta_i) = \sin(\theta_r) \Rightarrow \theta_i = \theta_r \quad \left(\begin{array}{l} \text{angle of incidence =} \\ \text{angle of reflection} \end{array} \right) \\
 \hat{E}_r &= -\hat{E}_i \\
 \hat{E}_i = E_i(\text{real}) &\Rightarrow E_y(x, z, t) = \text{Re} \left[\hat{E}_i \left(e^{-jk_z z} - e^{+jk_z z} \right) e^{j(\omega t - k_x x)} \right] \\
 &= 2E_i \sin(k_z z) \sin(\omega t - k_x x) \\
 \bar{H}(x, z, t) &= \text{Re} \left[\frac{\hat{E}_i}{\eta} \left[\cos(\theta) \left(-e^{-jk_z z} - e^{+jk_z z} \right) \bar{i}_x + \sin(\theta) \left(e^{-jk_z z} - e^{+jk_z z} \right) \bar{i}_z \right] \right. \\
 &\quad \left. \cdot e^{j(\omega t - k_x x)} \right] \\
 &= \frac{2E_i}{\eta} \left[-\cos(\theta) \cos(k_z z) \cos(\omega t - k_x x) \bar{i}_x \right. \\
 &\quad \left. + \sin(\theta) \sin(k_z z) \sin(\omega t - k_x x) \bar{i}_z \right]
 \end{aligned}$$

$$K_y(x, z = 0, t) = -H_x(x, z = 0, t) = \frac{2E_i}{\eta} \cos(\theta) \cos(\omega t - k_x x)$$

$$\langle \bar{S} \rangle = \frac{1}{2} \text{Re} \left[\hat{\bar{E}} \times \hat{H}^* \right] = \frac{2E_i^2}{\eta} \sin(\theta) \sin^2(k_z z) \bar{i}_x$$

B. \bar{H} Field Parallel to Interface (TM - Transverse Magnetic)

$$\bar{E}_i = \text{Re} \left[\hat{E}_i (\cos(\theta_i) \bar{i}_x - \sin(\theta_i) \bar{i}_z) e^{j(\omega t - k_{xi}x - k_{zi}z)} \right]$$

$$\bar{H}_i = \text{Re} \left[\frac{\hat{E}_i}{\eta} e^{j(\omega t - k_{xi}x - k_{zi}z)} \bar{i}_y \right]$$

$$\bar{E}_r = \text{Re} \left[\hat{E}_r (-\cos(\theta_r) \bar{i}_x - \sin(\theta_r) \bar{i}_z) e^{j(\omega t - k_{xr}x + k_{zr}z)} \right]$$

$$\bar{H}_r = \text{Re} \left[\frac{\hat{E}_r}{\eta} e^{j(\omega t - k_{xr}x - k_{zr}z)} \bar{i}_y \right]$$

$$E_x(x, z = 0, t) = 0 \Rightarrow \hat{E}_i \cos(\theta_i) e^{-jk_{xi}x} - \hat{E}_r \cos(\theta_r) e^{-jk_{xr}x} = 0$$

$$k_{xi} = k_{xr} \Rightarrow \sin(\theta_i) = \sin(\theta_r) \Rightarrow \theta_i = \theta_r$$

$$\hat{E}_i = \hat{E}_r$$

$$\hat{E}_i = E_i \text{ (real)} \Rightarrow \bar{E} = \text{Re} \left[\hat{E}_i \left[\cos(\theta) \left(e^{-jk_z z} - e^{+jk_z z} \right) \bar{i}_x - \sin(\theta) \left(e^{-jk_z z} + e^{+jk_z z} \right) \bar{i}_z \right] e^{j(\omega t - k_x x)} \right]$$

$$= 2E_i [\cos(\theta) \sin(k_z z) \sin(\omega t - k_x x) \bar{i}_x - \sin(\theta) \cos(k_z z) \cos(\omega t - k_x x) \bar{i}_z]$$

$$\bar{H} = \text{Re} \left[\frac{\hat{E}_i}{\eta} \left(e^{-jk_z z} + e^{+jk_z z} \right) e^{j(\omega t - k_x x)} \bar{i}_y \right]$$

$$= \frac{2E_i}{\eta} \cos(k_z z) \cos(\omega t - k_x x) \bar{i}_y$$

$$K_x(x, z = 0) = H_y(x, z = 0) = \frac{2E_i}{\eta} \cos(\omega t - k_x x)$$

$$\sigma_s(x, z = 0) = -\epsilon E_z(x, z = 0) = 2\epsilon E_i \sin(\theta) \cos(\omega t - k_x x)$$

Check: Conservation of Charge

$$\underbrace{\nabla_{\Sigma} \cdot \bar{K}}_{\text{surface divergence}} + \frac{\partial \sigma_s}{\partial t} = 0 \Rightarrow \frac{\partial K_x}{\partial x} + \frac{\partial \sigma_s}{\partial t} = 0$$

$$\langle \bar{S} \rangle = \frac{1}{2} \text{Re} \left(\hat{\bar{E}} \times \hat{H}^* \right) = \frac{2E_i^2}{\eta} \sin(\theta) \cos^2(k_z z) \bar{i}_x$$

III. Oblique Incidence Onto a Dielectric

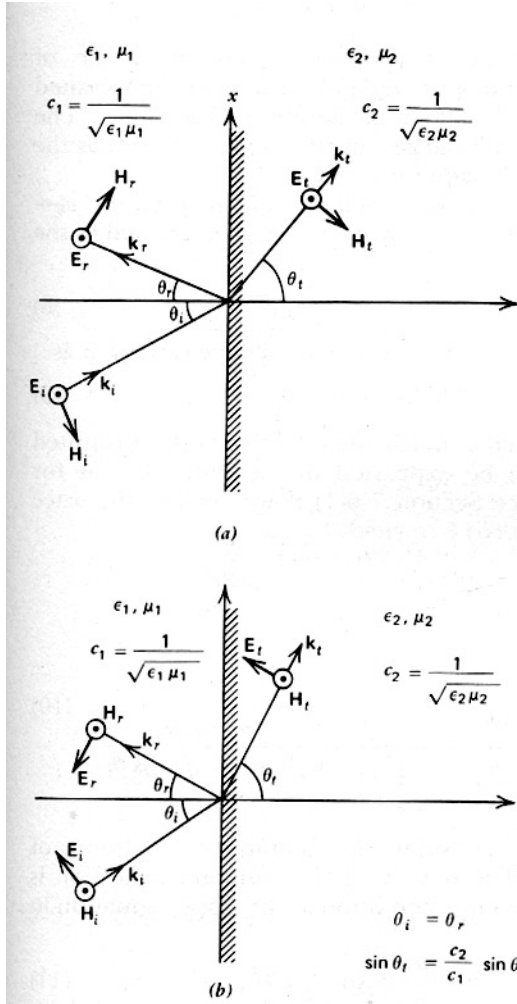


Figure 7-18 A uniform plane wave obliquely incident upon a dielectric interface also has its angle of incidence equal to the angle of reflection while the transmitted angle is given by Snell's law. (a) Electric field polarized parallel to the interface. (b) Magnetic field parallel to the interface.

From *Electromagnetic Field Theory: A Problem Solving Approach*, by Markus Zahn, 1987. Used with permission.

A. TE ($\vec{E} \parallel$ Interface) Waves

$$\begin{aligned} \bar{E}_i &= \text{Re} \left[\hat{E}_i e^{j(\omega t - k_{xi}x - k_{zi}z)} \bar{i}_y \right] \\ \bar{H}_i &= \text{Re} \left[\frac{\hat{E}_i}{\eta_1} (-\cos(\theta_i) \bar{i}_x + \sin(\theta_i) \bar{i}_z) e^{j(\omega t - k_{xi}x - k_{zi}z)} \right] \\ \bar{E}_r &= \text{Re} \left[\hat{E}_r e^{j(\omega t - k_{xr}x + k_{zr}z)} \bar{i}_y \right] \\ \bar{H}_r &= \text{Re} \left[\frac{\hat{E}_r}{\eta_1} (\cos(\theta_r) \bar{i}_x + \sin(\theta_r) \bar{i}_z) e^{j(\omega t - k_{xr}x + k_{zr}z)} \right] \\ \bar{E}_t &= \text{Re} \left[\hat{E}_t e^{j(\omega t - k_{xt}x - k_{zt}z)} \bar{i}_y \right] \\ \bar{H}_t &= \text{Re} \left[\frac{\hat{E}_t}{\eta_2} (-\cos(\theta_t) \bar{i}_x + \sin(\theta_t) \bar{i}_z) e^{j(\omega t - k_{xt}x - k_{zt}z)} \right] \end{aligned}$$

$$\begin{aligned}
k_{xi} &= k_1 \sin(\theta_i) & k_{xr} &= k_1 \sin(\theta_r) & k_{xt} &= k_2 \sin(\theta_t) \\
k_{zi} &= k_1 \cos(\theta_i) & k_{zr} &= k_1 \cos(\theta_r) & k_{zt} &= k_2 \cos(\theta_t) \\
k_1 &= \frac{\omega}{c_1} = \omega \sqrt{\epsilon_1 \mu_1} & k_2 &= \frac{\omega}{c_2} = \omega \sqrt{\epsilon_2 \mu_2} \\
c_1 &= \frac{1}{\sqrt{\epsilon_1 \mu_1}} & c_2 &= \frac{1}{\sqrt{\epsilon_2 \mu_2}} \\
\eta_1 &= \sqrt{\frac{\mu_1}{\epsilon_1}} & \eta_2 &= \sqrt{\frac{\mu_2}{\epsilon_2}}
\end{aligned}$$

$$\begin{aligned}
E_y(z=0_-) &= E_y(z=0_+) \Rightarrow \hat{E}_i e^{-jk_{xi}x} + \hat{E}_r e^{-jk_{xr}x} = \hat{E}_t e^{-jk_{xt}x} \\
H_x(z=0_-) &= H_x(z=0_+) \Rightarrow \frac{1}{\eta_1} \left(-\hat{E}_i \cos(\theta_i) e^{-jk_{xi}x} + \hat{E}_r \cos(\theta_r) e^{-jk_{xr}x} \right) \\
&= -\frac{1}{\eta_2} \hat{E}_t \cos(\theta_t) e^{-jk_{xt}x}
\end{aligned}$$

$$\begin{aligned}
k_{xi} = k_{xr} = k_{xt} &\Rightarrow k_1 \sin(\theta_i) = k_1 \sin(\theta_r) = k_2 \sin(\theta_t) \\
\theta_i &= \theta_r
\end{aligned}$$

$$\sin(\theta_t) = \frac{k_1}{k_2} \sin(\theta_i) = \frac{\cancel{\omega} c_2}{\cancel{\omega} c_1} \sin(\theta_i) = \frac{c_2}{c_1} \sin(\theta_i) \quad (\text{Snell's Law})$$

$$\begin{aligned}
\text{Index of refraction:} \quad n &= \frac{c_0}{c} = \frac{\sqrt{\epsilon \mu}}{\sqrt{\epsilon_0 \mu_0}} = \sqrt{\epsilon_r \mu_r} \\
\sin(\theta_t) &= \frac{n_1}{n_2} \sin(\theta_i)
\end{aligned}$$

$$\text{Reflection Coefficient:} \quad R = \frac{\hat{E}_r}{\hat{E}_i} = \frac{\frac{\eta_2}{\cos(\theta_t)} - \frac{\eta_1}{\cos(\theta_i)}}{\frac{\eta_2}{\cos(\theta_t)} + \frac{\eta_1}{\cos(\theta_i)}} = \frac{\eta_2 \cos(\theta_i) - \eta_1 \cos(\theta_t)}{\eta_2 \cos(\theta_i) + \eta_1 \cos(\theta_t)}$$

$$\text{Transmission Coefficient:} \quad T = \frac{\hat{E}_t}{\hat{E}_i} = \frac{2\eta_2}{\cos(\theta_t) \left(\frac{\eta_2}{\cos(\theta_t)} + \frac{\eta_1}{\cos(\theta_i)} \right)} = \frac{2\eta_2 \cos(\theta_i)}{\eta_2 \cos(\theta_i) + \eta_1 \cos(\theta_t)}$$

B. Brewster's Angle of No Reflection

$$R = 0 \Rightarrow \eta_2 \cos(\theta_i) = \eta_1 \cos(\theta_t)$$

$$\eta_2^2 \cos^2(\theta_i) = \eta_2^2 (1 - \sin^2(\theta_i)) = \eta_1^2 \cos^2(\theta_t) = \eta_1^2 (1 - \sin^2(\theta_t)) = \eta_1^2 \left(1 - \frac{c_2^2}{c_1^2} \sin^2(\theta_i) \right)$$

$$\sin^2(\theta_i) \left(\frac{\eta_1^2 c_2^2}{c_1^2} - \eta_2^2 \right) = \eta_1^2 - \eta_2^2$$

$$\sin^2(\theta_i) \left[\frac{\mu_1 \cancel{\epsilon_1} \mu_1}{\cancel{\epsilon_1} \epsilon_2 \mu_2} - \frac{\mu_2}{\epsilon_2} \right] = \frac{\mu_1}{\epsilon_1} - \frac{\mu_2}{\epsilon_2}$$

$$\sin^2(\theta_i) = \sin^2(\theta_B) = \frac{1 - \frac{\epsilon_2 \mu_1}{\epsilon_1 \mu_2}}{1 - \left(\frac{\mu_1}{\mu_2} \right)^2}$$

θ_B is called the Brewster angle. There is no Brewster angle for TE polarization if $\mu_1 = \mu_2$.

C. Critical Angle of No Power Transmission

If $c_2 > c_1$, $\sin(\theta_t)$ can be greater than 1:

$$\sin(\theta_t) = \frac{c_2}{c_1} \sin(\theta_i)$$

$$\theta_i = \theta_c \Rightarrow \sin(\theta_i) = \frac{c_1}{c_2} \quad (\text{Real solution for } \theta_i \text{ if } c_1 < c_2)$$

θ_c is called the critical angle. At the critical angle, $\theta_t = \frac{\pi}{2} \Rightarrow k_{zt} = k_2 \cos(\theta_t) = 0$.

For $\theta_i > \theta_c$, $\sin(\theta_t) > 1 \Rightarrow \cos(\theta_t) = \sqrt{1 - \sin^2(\theta_t)} \Rightarrow -j\alpha = k_{zt}$

$$\begin{aligned}\bar{E}_t &= \text{Re} \left[\hat{E}_t e^{j(\omega t - k_{xt}x)} e^{-\alpha z} \bar{i}_y \right] \\ \bar{H}_t &= \text{Re} \left[\frac{\hat{E}_t}{\eta_2} (-\cos(\theta_t) \bar{i}_x + \sin(\theta_t) \bar{i}_z) e^{j(\omega t - k_{xt}x)} e^{-\alpha z} \right]\end{aligned}$$

These are non-uniform plane waves.

$$\begin{aligned}\langle S_z \rangle &= -\frac{1}{2} \text{Re} \left[\hat{E}_y \hat{H}_x^* \right] = -\frac{1}{2} \text{Re} \left[\frac{\hat{E}_t \hat{E}_t^*}{\eta_2} (-\cos(\theta_t))^* e^{-2\alpha z} \right] \\ &= 0 \quad \left(\cos(\theta_t) = -\frac{j\alpha}{k_2} \right)\end{aligned}$$

D. TM ($\bar{H} \parallel$ interface) Waves

$$\begin{aligned}\bar{E}_i &= \text{Re} \left[\hat{E}_i (\cos(\theta_i) \bar{i}_x - \sin(\theta_i) \bar{i}_z) e^{j(\omega t - k_{xi}x - k_{zi}z)} \right] \\ \bar{H}_i &= \text{Re} \left[\frac{\hat{E}_i}{\eta_1} e^{j(\omega t - k_{xi}x - k_{zi}z)} \bar{i}_y \right] \\ \bar{E}_r &= \text{Re} \left[\hat{E}_r (-\cos(\theta_r) \bar{i}_x - \sin(\theta_r) \bar{i}_z) e^{j(\omega t - k_{xr}x + k_{zr}z)} \right] \\ \bar{H}_r &= \text{Re} \left[\frac{\hat{E}_r}{\eta_1} e^{j(\omega t - k_{xr}x + k_{zr}z)} \bar{i}_y \right] \\ \bar{E}_t &= \text{Re} \left[\hat{E}_t (\cos(\theta_t) \bar{i}_x - \sin(\theta_t) \bar{i}_z) e^{j(\omega t - k_{xt}x - k_{zt}z)} \right] \\ \bar{H}_t &= \text{Re} \left[\frac{\hat{E}_t}{\eta_2} e^{j(\omega t - k_{xt}x - k_{zt}z)} \bar{i}_y \right]\end{aligned}$$

$$\begin{aligned}E_x(x, z = 0_-, t) = E_x(x, z = 0_+, t) &\Rightarrow \hat{E}_i \cos(\theta_i) e^{-jk_{xi}x} - \hat{E}_r \cos(\theta_r) e^{-jk_{xr}x} = \hat{E}_t \cos(\theta_t) e^{-jk_{xt}x} \\ H_y(x, z = 0_-, t) = H_y(x, z = 0_+, t) &\Rightarrow \frac{1}{\eta_1} \left(\hat{E}_i e^{-jk_{xi}x} + \hat{E}_r e^{-jk_{xr}x} \right) = \frac{1}{\eta_2} \hat{E}_t e^{-jk_{xt}x}\end{aligned}$$

$$k_{xi} = k_{xr} = k_{xt} \Rightarrow \theta_i = \theta_r$$

$$\sin(\theta_t) = \frac{c_2}{c_1} \sin(\theta_i) \quad (\text{Snell's Law})$$

$$R = \frac{\hat{E}_r}{\hat{E}_i} = \frac{\eta_1 \cos(\theta_i) - \eta_2 \cos(\theta_t)}{\eta_2 \cos(\theta_t) + \eta_1 \cos(\theta_i)}$$

$$T = \frac{\hat{E}_t}{\hat{E}_i} = \frac{2\eta_2 \cos(\theta_i)}{\eta_2 \cos(\theta_t) + \eta_1 \cos(\theta_i)}$$

Brewster's Angle:

$$\begin{aligned}
 R = 0 &\Rightarrow \eta_1 \cos(\theta_i) = \eta_2 \cos(\theta_t) \\
 \eta_1^2 \cos^2(\theta_i) &= \eta_1^2(1 - \sin^2(\theta_i)) = \eta_2^2 \cos^2(\theta_t) = \eta_2^2(1 - \sin^2(\theta_t)) \\
 &= \eta_2^2 \left(1 - \frac{c_2^2}{c_1^2} \sin^2(\theta_i) \right) \\
 \sin^2(\theta_i) \left[\frac{\eta_2^2 c_2^2}{c_1^2} - \eta_1^2 \right] &= \eta_2^2 - \eta_1^2 \\
 \sin^2(\theta_i) \left[\frac{\cancel{\mu_2} \epsilon_1 \mu_1}{\epsilon_2 \epsilon_2 \cancel{\mu_2}} - \frac{\mu_1}{\epsilon_1} \right] &= \frac{\mu_2}{\epsilon_2} - \frac{\mu_1}{\epsilon_1} \\
 \sin^2(\theta_i) &= \sin^2(\theta_B) = \frac{1 - \frac{\epsilon_1 \mu_1}{\epsilon_2 \mu_2}}{1 - \left(\frac{\epsilon_1}{\epsilon_2} \right)^2}
 \end{aligned}$$

If $\mu_1 = \mu_2$:

$$\begin{aligned}
 \sin^2(\theta_B) &= \frac{1}{1 + \frac{\epsilon_1}{\epsilon_2}} \Rightarrow \tan(\theta_B) = \sqrt{\frac{\epsilon_2}{\epsilon_1}} \\
 \theta_B + \theta_t &= \frac{\pi}{2} \\
 \frac{1}{\sin^2(\theta_B)} &= \frac{1}{\sin^2(\theta_C)} + 1 \Rightarrow \theta_C > \theta_B
 \end{aligned}$$